



German OpenFOAM User meeting 2017 (GOFUN 2017) Particle Simulation with OpenFOAM® Introduction, Fundamentals and

**Applications** 

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### Outline

#### Introduction

Motivation Lagrangian-Particle-Tracking in OpenFOAM

#### Fundamentals of Lagrangian-Particle-Tracking

Governing Equations Particle Forces Particle Response Time Phase-Coupling Mechanisms Particle-Particle Interaction

#### Application

How to build your own Eulerian-Lagrangian Solver in OpenFOAM How to use your own Eulerian-Lagrangian Solver in OpenFOAM Post-Processing with OpenFOAM/Paraview





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### Why Particle Simulations with OpenFOAM?

- OpenFOAM is free and open source (customization and unlimited parallelization possible)
- OpenFOAM is constantly under development with a continuous growing community (academic research, R&D in companies)
- OpenFOAM includes solvers for any application of particle-laden flows (e.g. process engineering, mechanical engineering, civil engineering, physics,...)







## Lagrangian-Particle-Tracking in OpenFOAM

- Solvers for any kind of particle-laden flow are already implemented<sup>1</sup>:
  - DPMFoam/MPPICFoam: Transient solver for the coupled transport of a single kinematic particle cloud including the effect of the volume fraction of particles on the continuous phase (Multi-Phase Particle In Cell modeling is used to represent collisions without resolving particle-particle interactions)
  - uncoupledKinematicParcelFoam: Transient solver for the passive transport of a single kinematic particle cloud
  - reactingParcelFilmFoam: Transient solver for compressible, turbulent flow with a reacting, multiphase particle cloud, and surface film modelling
  - sprayFoam: Transient solver for compressible, turbulent flow with a spray particle cloud

No proper solver available? Customize one of the existing...

<sup>• ...</sup> 

<sup>&</sup>lt;sup>1</sup>based on OpenFOAM-4.x





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### Governing Equations of Lagrangian-Particle-Tracking

 Calculation of isothermal particle motions requires the solution of the following set of ordinary differential equations:

$$\frac{\mathrm{d}\mathbf{x}_{p}}{\mathrm{d}t} = \mathbf{u}_{p}, \qquad m_{p}\frac{\mathrm{d}\mathbf{u}_{p}}{\mathrm{d}t} = \sum \mathbf{F}_{i}, \qquad I_{p}\frac{\mathrm{d}\omega_{p}}{\mathrm{d}t} = \sum \mathbf{T}$$
(1)

 Newton's second law of motion presupposes the consideration of all relevant forces acting on the particle, e.g., drag, gravitational and buoyancy forces, pressure forces:

$$m_{\rho}\frac{\mathrm{d}\mathbf{u}_{\rho}}{\mathrm{d}t} = \sum \mathbf{F}_{i} = \mathbf{F}_{D} + \mathbf{F}_{G} + \mathbf{F}_{P} + \dots$$
(2)





## Drag Force

 Drag is the most important force (approx. 80 % of the total force) and is expressed in terms of the drag coefficient C<sub>D</sub>:

$$\mathbf{F}_{\mathbf{D}} = C_D \frac{\pi D_\rho^2}{8} \rho_f \left( \mathbf{u}_f - \mathbf{u}_\rho \right) \left| \mathbf{u}_f - \mathbf{u}_\rho \right|$$
(3)

### Drag correlations (spherical particle)

• Schiller-Naumann (1935):

$$C_D = \begin{cases} \frac{24}{{\sf Re}_p} \left(1 + 0.15 {\sf Re}_p^{0.687}\right) & \text{if } {\sf Re}_p \le 1000 \\ 0.44 & \text{if } {\sf Re}_p > 1000 \end{cases}$$

• Putnam (1961):

$$C_D = \left\{ egin{array}{c} rac{24}{{\sf Re}_p} \left(1+rac{1}{6}{\sf Re}_p^{2/3}
ight) & {
m if}\; {\sf Re}_p \leq 1000 \ 0.424 & {
m if}\; {\sf Re}_p > 1000 \end{array} 
ight.$$

(4)

(5)







Figure: Drag coefficient as a function of particle Reynolds number, comparison of experimental data with correlations of Schiller-Naumann (1935) and Putnam (1961)





### Gravity/Buoyancy and Pressure Gradient Force

· Gravitational and Buoyancy force is computed as one total force:

$$\mathbf{F}_{\mathbf{G}} = m_{\rho} \mathbf{g} \left( 1 - \frac{\rho_f}{\rho_{\rho}} \right) \tag{6}$$

• The force due to a local pressure gradient can be expressed for a spherical particle simply as:

$$\mathbf{F}_{\mathbf{P}} = -\frac{\pi D_{\rho}^3}{6} \nabla \rho \tag{7}$$

 Expressing the local pressure gradient ∇p in terms of the momentum equation leads to the final pressure gradient force:

$$\mathbf{F}_{\mathbf{p}} = \rho_f \frac{\pi D_{\mathbf{p}}^3}{6} \left( \frac{\mathsf{D}\mathbf{u}_f}{\mathsf{D}t} - \nabla \cdot \nu \left( \nabla \mathbf{u}_f + \nabla \mathbf{u}_f^T \right) \right)$$
(8)





### Other Forces

- Added mass force: particle acceleration or deceleration in a fluid requires also an accelerating or decelerating of a certain amount of the fluid surrounding the particle (important for liquid-particle flows)
- Slip-shear lift force: particles moving in a shear layer experience a transverse lift force due to the nonuniform relative velocity over the particle and the resulting nonuniform pressure distribution
- Slip-rotation lift force: particles, which are freely rotating in a flow, may also experience a lift force due to their rotation (Magnus force)
- Thermophoretic force: a thermal force moves fine particles in the direction of negative temperature gradients (important for gas-particle flows)







### Particle Response Time

- Particle response time is used to characterize the capability of particles to follow sudden velocity changes in the flow
- Starting from the equation of motion considering only drag force (divided by particle mass and in terms of the particle Reynolds number):

$$\frac{\mathrm{d}u_p}{\mathrm{d}t} = \frac{18\mu_f}{\rho_p D_p^2} \frac{C_D \operatorname{Re}_p}{24} (u_f - u_p) \rightarrow \frac{\mathrm{d}u_p}{\mathrm{d}t} = \frac{1}{\tau_p} (u_f - u_p) \tag{9}$$

Particle response time & Stokes number

$$\tau_{p} = \frac{\rho_{p} D_{p}^{2}}{18\mu_{f} f_{D}}, \quad \text{St} = \tau_{p} / \tau_{f} \qquad (10)$$



 $\rightarrow$  The Stokes number St is the ratio of the particle response time and a characteristic time scale of the flow

Figure: Graphical illustration of the particle response time (Sommerfeld, 2011)





### Phase-Coupling Mechanisms

- Phase-coupling mechanisms strongly influences the behavior of the continous and dispersed phase:
  - One-way coupling: fluid → particles
  - Two-way coupling: fluid ⇒ particles
  - Four-way coupling: fluid = particles + particle collisions
- Classification of phase-coupling mechanisms according to Elghobashi (1994):







## Particle-Particle Interaction

- OpenFOAM uses the soft-sphere-model (DSEM)
- Particle-particle collisions are considered using a spring, friction slider and dash-pot
- Normal force is expressed according to the Hertzian contact theory:

$$F_{n,ij} = \left(-k_n \delta_n^{3/2} - \eta_{n,j} \mathbf{G} \cdot \mathbf{n}\right) \mathbf{n} \qquad (11)$$

• Tangential force is expressed by:

$$F_{t,ij} = -k_n \delta_t - \eta_{t,j} \mathbf{G}_{ct}$$
 or (12)

$$F_{t,ij} = -\mu |\mathbf{F}_{n,ij}| \mathbf{t} \text{ if } |F_{t,ii}|_j > \mu |\mathbf{F}_{n,ij}|$$
 (13)







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- Problem: no proper solver is available for your requirements? 😊
- Solution: customize an existing solver for your own purposes! ③



Figure: Particle-laden backward-facing step flow according to Fessler & Eaton (1999)





- 1. Open a terminal and source OpenFOAM-4.x (if not already done)
- 2. Create a working directory for our Eulerian-Lagrangian solver and move into it:

mkdir solver/

cd solver/

- Copy the original pimpleFoam solver (Large time-step transient solver for incompressible, turbulent flow, using the PIMPLE (merged PISO-SIMPLE) algorithm) from OpenFOAM-4.x and rename it:
- cp -r \$FOAM\_SOLVERS/incompressible/pimpleFoam/ .
- mv pimpleFoam pimpleLPTFoam/

```
cd pimpleLPTFoam/
```





4. After moving into the pimpleLPTFoam directory, change the name of the pimpleFoam.C file, remove the pimpleDyMFoam and SRFPimpleFoam sub-solver directories:

```
mv pimpleFoam.C pimpleLPTFoam.C
```

```
rm -r pimpleDyMFoam/ SRFPimpleFoam/
```

```
mkdir lagrangian
```

- Copy the lagrangian library intermediate (includes submodels for particle forces, particle collisions, injection and dispersion models,...) from OpenFOAM-4.x:
- cp -r \$FOAM\_SRC/lagrangian/intermediate/ lagrangian/
  - 6. Open the createFields.H file with a text editor for some customizations:

```
vi createFields.H
```





 Add the following code lines after #include "createMRF.H" to create and read the fluid density from the transportProperties and calculate the inverse fluid density:

#### createFields.H

```
Info« "Reading transportProperties\n" « endl;
IOdictionary transportProperties
     IOobject
          "transportProperties",
          runTime.constant(),
          mesh.
          IOobject::MUST_READ_IF_MODIFIED,
          IOobject::NO_WRITE
):
dimensionedScalar rhoInfValue
     transportProperties.lookup("rhoInf")
);
dimensionedScalar invrhoInf("invrhoInf".(1.0/rhoInfValue)):
```





8. Create a volScalarField for the fluid density and the dynamic fluid viscosity:

#### createFields.H





9. Initialize the basicKinematicCollidingCloud (includes particle-particle interactions):

#### createFields.H

```
const word kinematicCloudName
(
    args.optionLookupOrDefault<word>("cloudName", "kinematicCloud")
);
Info« "Constructing kinematicCloud " « kinematicCloudName « endl;
basicKinematicCollidingCloud kinematicCloud
(
    kinematicCloudName,
    rhoInf,
    U,
    mu,
    g
);
```

### 10. Open the pimpleLPTFoam.C file for some customizations:

#### vi pimpleLPTFoam.C





11. Add the basicKinematicCollidingCloud.H and readGravitationalAcceleration.H to the existing header files:

#### pimpleLPTFoam.C

•••





12. Add the kinematicCloud.evolve() function after the PIMPLE corrector loop:

### pimpleLPTFoam.C

```
// -- Pressure-velocity PIMPLE corrector loop
while (pimple.loop())
     #include "UEqn.H"
     // -- Pressure corrector loop
     while (pimple.correct())
          #include "pEqn.H"
     if (pimple.turbCorr())
          laminarTransport.correct();
          turbulence->correct():
      ł
}
Info« "\nEvolving " « kinematicCloud.name() « endl;
kinematicCloud.evolve():
runTime.write():
```





13. Open the UEqn.H file for some customizations:

vi UEqn.H

14. Expand the momentum equation for two-way coupling:

### UEqn.H

```
tmp<fvVectorMatrix> tUEqn
(
    fvm::dt(U) + fvm::div(phi, U)
    + MRF.DDt(U)
    + turbulence->divDevReff(U)
    ==
    fvOptions(U)
    + invrhoInf*kinematicCloud.SU(U)
);
fvVectorMatrix& UEqn = tUEqn.ref();
UEqn.relax();
```





- 15. The implementation is (almost) done, but we need some customizations within the Make directory of the intermediate library in order to compile everything correctly:
- vi intermediate/Make/options
  - 16. We want our own customized intermediate library (maybe to implement a own particle force model or similar), so replace the last code line of the files file by:

#### files

- LIB = \$(FOAM\_USER\_LIBBIN)/libPimpleLPTLagrangianIntermediate
  - 17. Tell the solver where he can find our intermediate library (and some additional too):

#### vi Make/options





#### options

```
EXE_INC =
     -Ilagrangian/intermediate/lnInclude \
     -I$(LIB SRC)/TurbulenceModels/turbulenceModels/lnInclude \
     -I$(LIB_SRC)/TurbulenceModels/incompressible/lnInclude \
     -I$(LIB SRC)/transportModels \
     -I$(LIB_SRC)/transportModels/incompressible/singlePhaseTransportModel \
     -I$(LIB_SRC)/finiteVolume/lnInclude \
     -I$(LIB SRC)/meshTools/lnInclude \
     -I$(LIB_SRC)/sampling/lnInclude \
     -I$(LIB SRC)/lagrangian/basic/lnInclude \
     -I$(LIB SRC)/regionModels/surfaceFilmModels/lnInclude \
     -I$(LIB_SRC)/regionModels/regionModel/lnInclude
EXE LIBS = \setminus
     -L$(FOAM_USER_LIBBIN) \
     -lPimpleLPTLagrangianIntermediate \
     -llagrangian
     -lturbulenceModels \
     -lincompressibleTurbulenceModels \
     -lincompressibleTransportModels \setminus
     -lfiniteVolume \
```





18. Tell the compiler the name of our new Eulerian-Lagrangian solver:

vi Make/files

#### files

pimpleLPTFoam.C

EXE = \$(FOAM\_USER\_APPBIN)/pimpleLPTFoam

19. Finally, we can compile the intermediate library and the solver:

wmake all

### You received no error messages from the compiler? Congratulations, your new Eulerian-Lagrangian solver is ready... but how to use it? ⓒ





### Particle-laden backward-facing step flow (Fessler & Eaton, 1999)

- Geometry:
  - Step height: H = 26.7 mm
  - Channel height/width: h = 40 mm, B = 457 mm
  - Length inlet and expansion channel:  $L_U = 5h$ ,  $L_D = 35h$



- Flow and particle characteristics:
  - Centerline velocity and Reynolds number:  $U_0 = 10.5 \text{ m/s}$ , Re $_0 = U_0 H/\nu = 18.600$
  - Particle type: copper  $ightarrow D_{
    ho} =$  70  $\mu$ m,  $ho_{
    ho} =$  8800 kg/m<sup>3</sup>
  - Stokes number: St  $= rac{ au_p}{ au_f} = 
    ho_p D_p^2 U_0/(90 \mu H) = 6.9$







Figure: Snapshot of the instantaneous velocity field  $|\mathbf{U}|$  obtained from Large Eddy Simulation (sub-grid scale turbulence model: Dynamic Smagorinsky (DSM)) for Re<sub>0</sub> = 18.600





• Basic folder structure of any OpenFOAM case:

0: includes the initial boundary conditions

**constant:** includes the mesh (polyMesh folder), physical properties of the fluid (transportProperties), particle properties and settings (kinematicCloudProperties),....

**system:** includes the simulation settings (controlDict), settings for numerical schemes (fvSchemes) and solver for the algebraic equations systems (fvSolution), decomposition methods (decomposeParDict), ...

Download the current tutorial case setup using the git clone command:

#### Git repository on Bitbucket

\$ git clone https://slint@bitbucket.org/slint/gofun2017\_particletut.git





 We start with the mesh generation → move into the tutorial directory and build the 2D mesh using OpenFOAM's blockMesh utility and check the mesh quality:

cd gofun2017\_particletutorial/tutorial/BFS/

blockMesh

checkMesh



<u>,</u>

Figure: Two-dimensional block-structured mesh for the particle-laden backward-facing step flow





2. Let's see how to define initial boundary conditions (at the example of the velocity field):

### U dimensions [0 1 -1 0 0 0 0]; internalField uniform (0 0 0); boundaryField inlet type fixedValue: value uniform (9.39 0 0); outlet type zeroGradient: walls type noSlip: sides type empty;

- OpenFOAM needs the dimension of the flow field in SI-units (see OpenFOAM user guide)
- You can set an initial flow field if present
- Each patch needs an initial boundary condition
- Boundary conditions in OpenFOAM:
  - Dirichlet (fixedValue)
  - Neumann (fixedGradient/zeroGradient)
  - Special types: cyclic, symmetry, empty (for 2D caes), ...





Let's see how to set up the particle cloud:

### kinematicCloudProperties

solution

3

```
active true:
       coupled true;
       transient yes;
       cellValueSourceCorrection off;
       maxCo 0.3;
       interpolationSchemes
              rho cell:
              U cell:
              mu cell:
       integrationSchemes
              U Euler:
sourceTerms
       schemes
              U semiImplicit 1;
```

- Activate/de-activate the particle cloud ٠
- Enable/disable phase coupling
- Transient/steady-state solution (max. Courant number)
- Enable/disable correction of momentum transferred to the Eulerian phase
- Choose interpolation/integration ۲ schemes for the LPT and treatment of source terms





#### kinematicCloudProperties

```
constantProperties
{
    rho0 8800;
    youngsModulus 1.3e5;
    poissonstaio 0.35;
}
subModels
{
    particleForces
    {
        sphereDrag;
        gravity;
        pressureGradient
        {
            U U;
        }
    }
```

- Define the physical particle properties:
  - Density
  - Young's module (elastic modulus)
  - Poisson's ratio
- Define the relevant particle forces:
  - Drag force
  - Gravition/Buoyancy force
  - Pressure drag force





```
kinematicCloudProperties
injectionModels
       model1
              type patchInjection;
             patchName inlet;
             duration 1;
             parcelsPerSecond 33261;
             massTotal 0;
             parcelBasisType fixed;
             flowRateProfile constant 1;
             nParticle 1;
             SOT 0.4:
             UO (9.39 0 0);
             sizeDistribution
              Ł
                    type fixedValue;
                    fixedValueDistribution
                          value 0.00007:
             3
       3
```

- Setup of the particle injection:
  - Injection model + injection patch name
  - · Total duration of particle injection
  - Injected parcels/particles per second
  - Number of particles per parcel
  - Start-of-injection time (SOI)
  - Initial parcel/particle velocity (U<sub>0</sub>)
  - Size distribution model (normal size distribution, ...)





#### kinematicCloudProperties

dispersionModel none;

```
patchInteractionModel
standardWallInteraction;
```

```
standardWallInteractionCoeffs
{
```

```
type rebound;
e 0.97;
mu 0.09;
```

```
}
```

```
surfaceFilmModel none;
```

```
stochasticCollisionModel none;
```

```
collisionModel pairCollision;
```

- Specify the sub-models for the particle simulation:
  - Turbulent dispersion models (Discrete Random Walk model and Gradient Dispersion model)
  - Patch interaction model + coefficients (rebound, stick or escape)
  - Surface film model for dripping and film interaction (absorb, bounce and splash)
  - Stochastic collision/pair collision model (spring, slider and dash-pot)
  - Further sub-models: heat transfer (only Ranz-Marshall correlation), phase change,...





#### kinematicCloudProperties

```
pairCollisionCoeffs
       maxInteractionDistance 0.00007:
       writeReferredParticleCloud no;
       pairModel pairSpringSliderDashpot;
       pairSpringSliderDashpotCoeffs
              useEquivalentSize no;
              alpha 0.12;
              b 1.5;
              mu 0.52:
              cohesionEnergyDensity 0:
              collisionResolutionSteps 12:
       1:
       wallModel wallSpringSliderDashpot:
       wallSpringSliderDashpotCoeffs
              useEquivalentSize no:
              collisionResolutionSteps 12:
              voungsModulus 1e10:
              poissonsRatio 0.23:
              alpha 0.12:
              b 1.5;
              mu 0.43;
              cohesionEnergyDensity 0;
       };
```

- Adjust the particle-particle and particle-wall interaction model coefficients:
  - *α*: coefficient related to the coefficient of restitution *e* (see diagram)
  - b: Spring power  $\rightarrow b = 1$  (linear) or b = 3/2 (Hertzian theory)
  - μ: friction coefficient



Figure: Relationship between  $\alpha$  and the coefficient of restitution *e* (Tsuji et al., 1992)





kinematicCloudProperties
<pre>cloudFunctions {     voidFraction1     {         type voidFraction;     } </pre>
}

• Use cloudFunctions to record particle tracks, calculate particle erosion, ...

4. The last step is to define the vector of the gravitational acceleration:



5. Finally, start our solver (and write a log file):

```
pimpleLPTFoam > run.log &
```





6. Use OpenFOAM's foamMonitor utility to check the convergence:

foamMonitor -l postProcessing/residuals/0/residuals.dat







## Post-Processing with OpenFOAM/Paraview

- OpenFOAM provides many utilities (e.g. sampling of data) and functionObjects (e.g. calculation of forces and turbulence fields) for the analysis of simulation results
- The standard program for the graphical post-processing of OpenFOAM cases is Paraview (see OpenFOAM user guide)
- 1. Start post-processing with Paraview by typing:

paraFoam

2. Load the last time step and check the velocity and pressure field:







### Post-Processing with OpenFOAM/Paraview



3. Let's check how much volume of each grid cell is occupied by particles (void fraction  $\alpha = V_{\rm P}/V_{\rm c}$ ):







### Post-Processing with OpenFOAM/Paraview

 Apply the Extract Block filter on the kinematicCloud and scale the particles using the Glyph filter:



 Sample the flow and particle velocity using OpenFOAM's sample utility (see OpenFOAM user guide) and plot the velocity profiles:







### Further Information and References



OpenFOAM User/Programmers Guide (www.openfoam.org)



Crow, T. C., Schwarzkopf, J. D., Sommerfeld, M. and Tsuji, Y., 2011, Multiphase flows with droplets and particles, 2nd ed., CRC Press, Taylor & Francis,



Sommerfeld, M., 2010, Particle Motion in Fluids, VDI Heat Atlas, Springer,



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- Fessler, J. R. and Eaton, J. K., 1999, Turbulence modification by particles in a backward-facing step flow, J. Fluid Mech., Vol. 394, pp. 97-117.
- Tsuji, Y., Tanaka, T. and Ishida, T., 1992, Lagrangian numerical simulation of plug flow of collisionless particles in a horizontal pipe. Powder Tech., Vol. 71, 239.





### Thank you for your attention!

### Any questions?

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