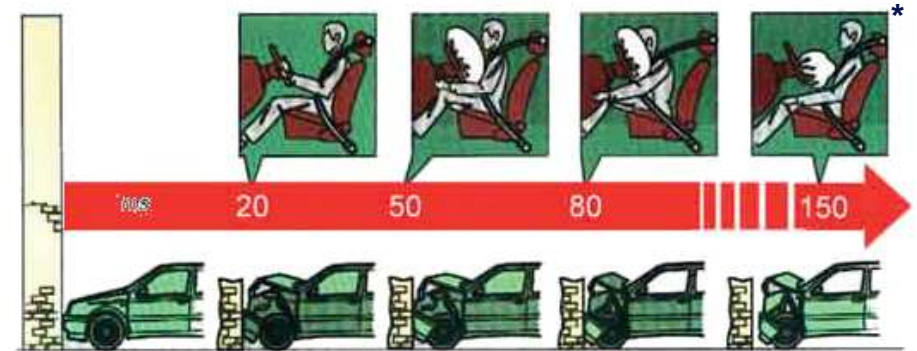


27th February 2019

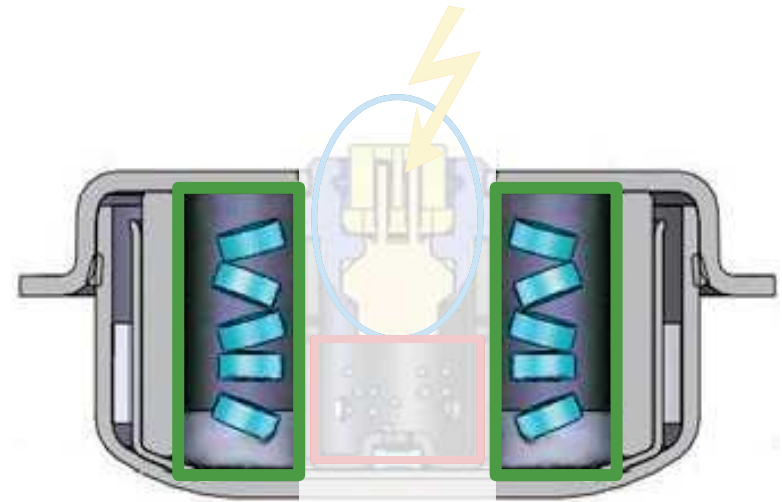
Modeling of solid propellant burning procedure in inflator relevant applications

Tilo Laufer, EMEA Safety Systems Numerical Simulation





- more than 10 Airbags in modern premium cars
- a3ms injury criteria allows up to 80G's
- Red Bull Air Race plane pilot experiences a maximum of 10G's

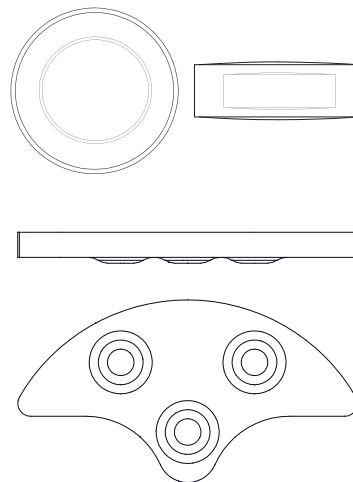


- fill a 60L airbag within 30ms with 1.5bar absolute pressure
- **initiator**, transfers an electric signal into a chemical reaction
- **booster**, enhances the initiator reaction
- **combustion-chamber**, produces a large amount of fluid to fill an airbag

- inflator development is accompanied by many difficulties
 - non steady state behavior
 - short time span of approx. 50ms
 - one can't look inside the inflator during combustion



- only very few testing data
 - pressure can be measured
 - difficult temperature measurement
 - no velocity measurement
- current approach
 - analytical description of model
 - average pressure
 - ideal gas
 - adiabatic system



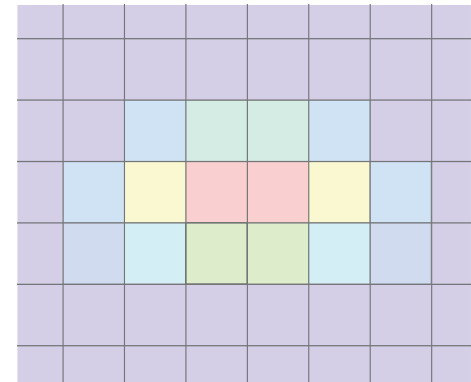
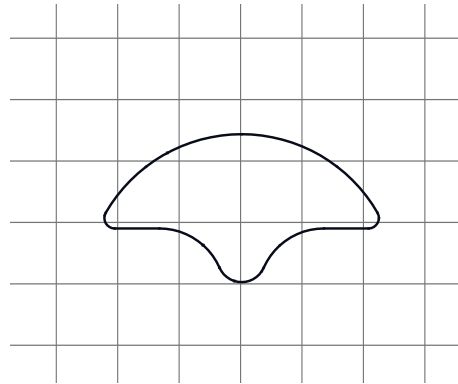
I. interface tracking

II. propellant BC

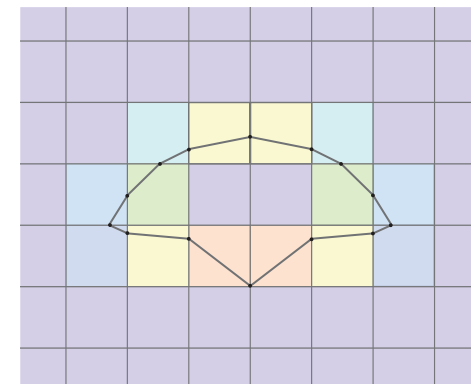
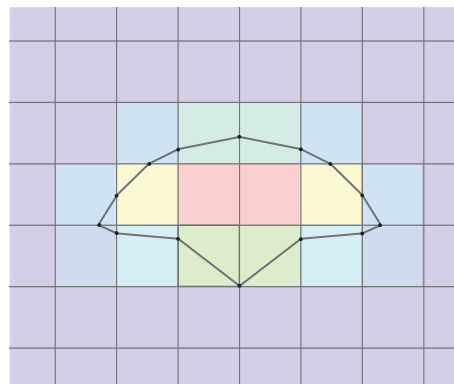
III. combustion modeling

- Introduction of volScalarField lambda

$$\lambda = \frac{V_{\text{propellant}}}{V_{\text{propellant}} + V_{\text{fluid}}}$$



- reconstruction of propellant surface:
 - IsoAdvect - Lib*



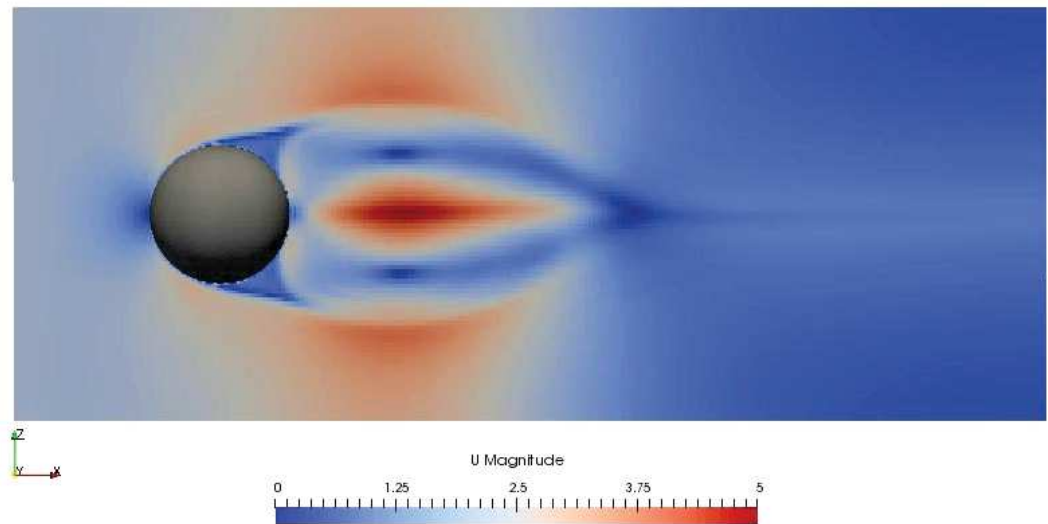
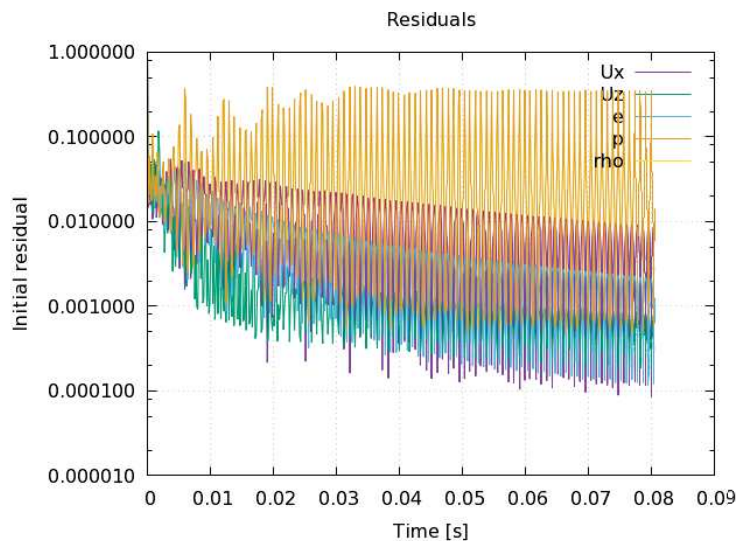
I. interface tracking

II. propellant BC

III. combustion modeling

- Using Immersed boundary method (IBM) to apply boundary conditions (BC) of the propellant onto the flow field
- openHFDIB - Lib*
- Problems with PISO-based algorithms
- e.g. rhoPimpleFoam

Time: 80.0 ms

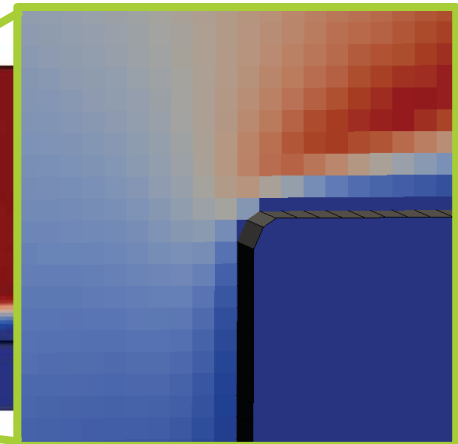
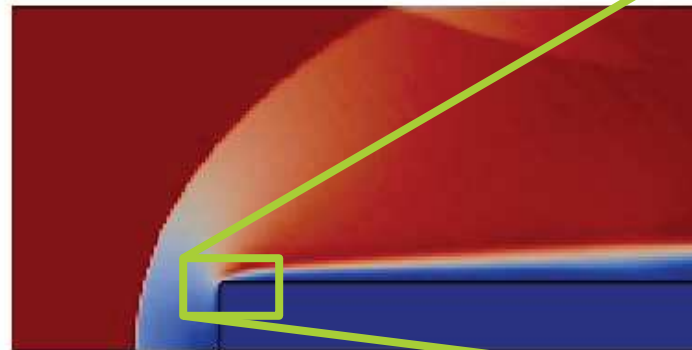


* „A Hybrid Fictitious Domain-Immersed Boundary Method for the Direct Simulation of Heat and Mass Transport in Fluid-Particle Systems“ by F. Municchi, S. Radl & C. Goniva

- Applying IBM on rhoCentralFoam-Solver
forwardstep – case

Time: 0.75 s

U Magnitude



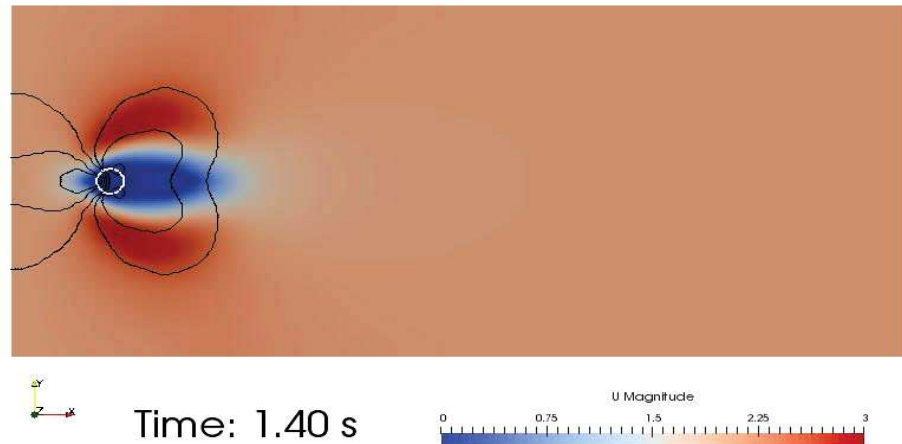
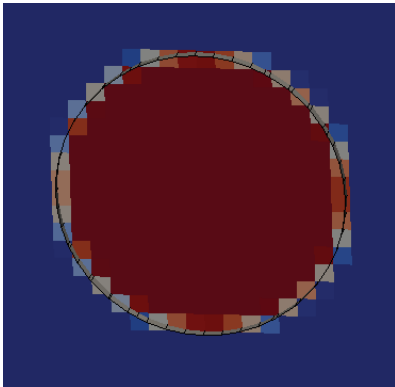
I. interface tracking

II. propellant BC

III. combustion modeling

- Propellant surface is defined by volScalarField lambda
- lambda has to change

```
lambda = max(lambda - dot_r * deltaT, 0.0);
```



- Set of governing equations by Clarke & Lowe*

$$\frac{d}{dt} \int_V U dV = - \int_A F_j n_j dA + \int_V (S_{ch} + S_a) dV$$

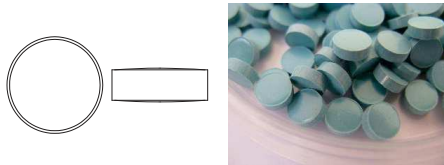
$$U = \begin{pmatrix} \rho \\ \rho c^\alpha \\ \rho u_i \\ \rho E \end{pmatrix}, \quad F_j = \begin{pmatrix} \rho u_j \\ \rho u_j c^\alpha \\ \rho u_j u_i + p \\ \rho u_j (E + pv) \end{pmatrix}, \quad S_{ch} = \begin{pmatrix} 0 \\ \mathfrak{R}^\alpha \\ 0 \\ 0 \end{pmatrix}, \quad S_a = \begin{pmatrix} \dot{M} \\ \dot{M}^\alpha \\ \dot{F} \\ \dot{H} \end{pmatrix}$$

- With the sources:

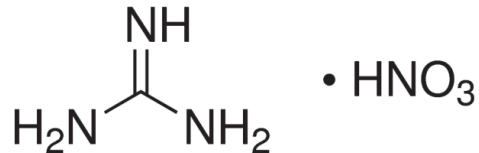
$$\begin{aligned} \dot{M} &= \dot{r} \rho_{\text{propellant}} \\ \dot{F} &= 0 \quad \because \quad u_{\text{fluid}} \gg u_{\text{surf}} \\ \dot{H} &= \dot{M} e_{\text{heat of explosion}} \end{aligned}$$

- current state of research

- Applying derived solver onto closed vessel test
- Volume $\approx 18\text{cm}^3$
- Cylinder shaped propellant

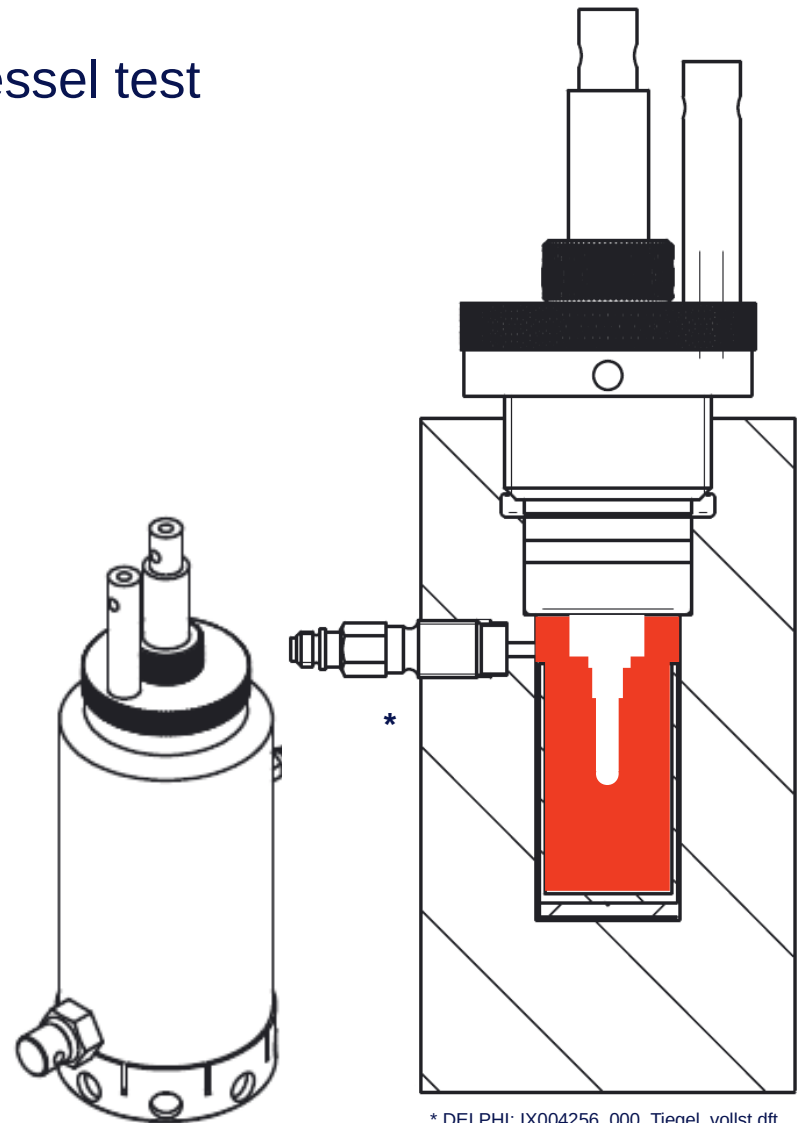


- 2.5g of Guanidine nitrate propellant



- Analytical Solutions suggest

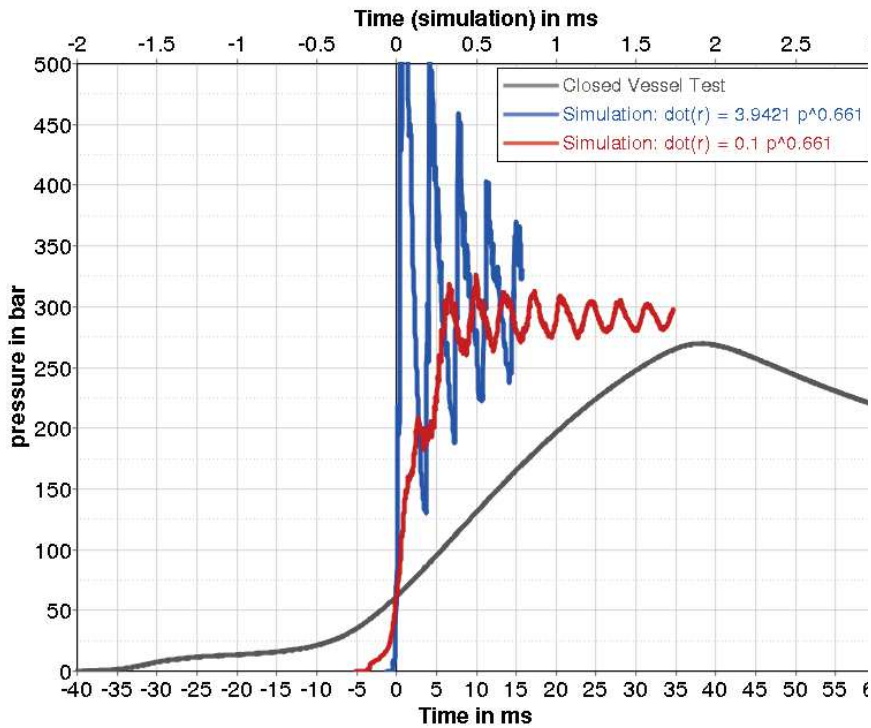
$$\begin{aligned} \dot{r} &= B p^n \\ B &= 3.9421 \\ n &= 0.661 \end{aligned}$$



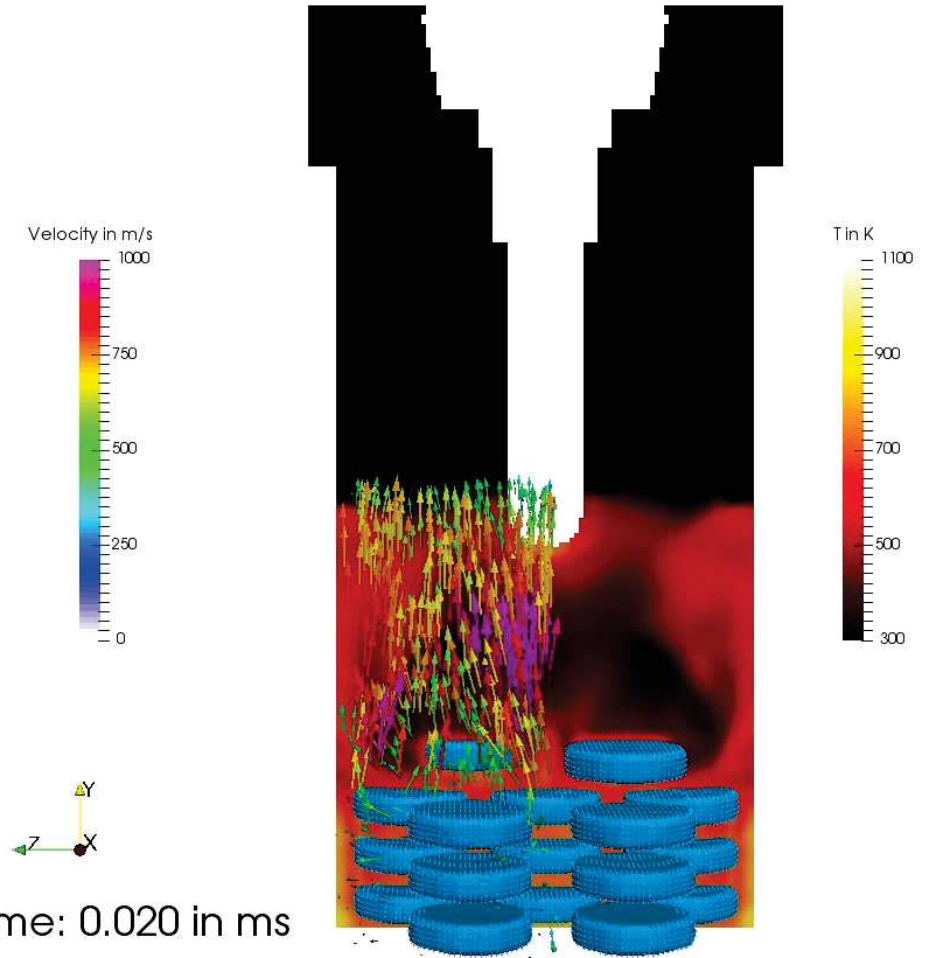
* DELPHI: IX004256_000_Tiegel_vollst.dft

- Results based on analytical derived combustion law

Closed Vessel pressure



Time: 0.020 in ms



- Summary:
 - proof of concept
 - OpenFOAM is capable of simulating solid propellant combustion
 - Code works in 2D as well as in 3D cases
- Outlook:
 - validation of methods
 - adding chemistry based combustion
 - Apply CFD simulations onto real inflator related applications

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Thank you for your attention!

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